

CINEMATIC ANALYSIS OF FIRST LINE BRAKING MECHANISM OF COOLING BED AT SMALL PROFILE ROLLING MILLS

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ABSTRACT:

In this paper is presented a study about cinematic analysis of first line braking mechanism, component part of cooling bed at small profile rolling mills.

CUVINTE CHEIE/KEYWORDS:

cinematic analysis, cooling bed, braking mechanism

1. INTRODUCTION

The cooling beds of small profile rolling mills have a very important role in obtaining of a finite product of a high quality. These cooling beds assure a conducted cooling of laminated profiles at the same time wish straightening them during the crossing of the cooling bed fiability, a diminution of exploitation costs.

2. CINEMATIC ANALYSIS OF MECHANISM

This mechanism is a plane mechanism, with a single motor element. This is based of four bar mechanism ABCD, four bar mechanism DCEG, four bar mechanism GEFI. Between elements EG- GH and FI-IK is established an 81° fixed angle. Mechanism is presented in initial position.

Structural decomposition of first line braking mechanism is presented in figure 1, and cinematic scheme is presented in figure 2.

Angle between extreme positions is 47° , and node path corresponding on complete rotation of motor element is presented in figure 3.

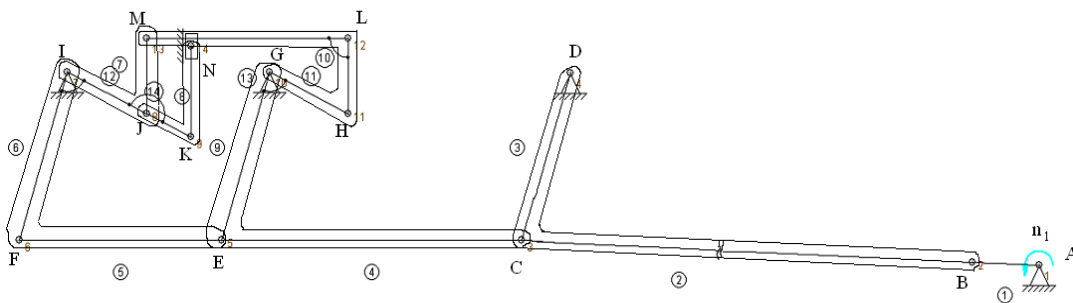


Fig. 1. Structural decomposition of mechanism

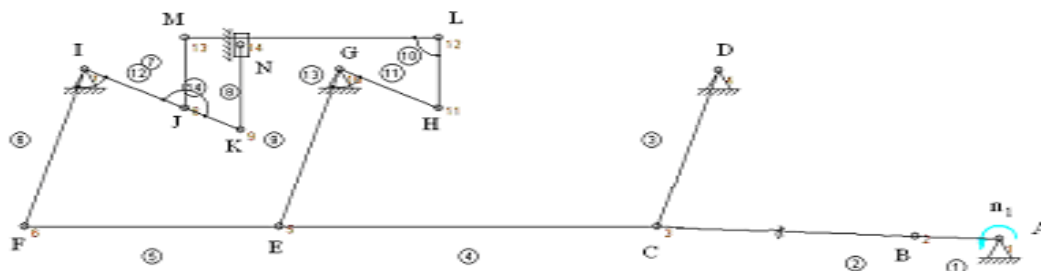


Fig. 2. Cinematic scheme of first braking mechanism

Element length and angular velocity for motor element is:

$l_1 = 143 \text{ mm}$	$l_2 = 1800 \text{ mm}$	$l_3 = 350 \text{ mm}$
$l_4 = 640 \text{ mm}$	$l_5 = 430 \text{ mm}$	$l_6 = 350 \text{ mm}$
$l_7 = 150 \text{ mm}$	$l_8 = 105 \text{ mm}$	$l_9 = 350 \text{ mm}$
$l_{10} = 150 \text{ mm}$	$l_{11} = 187 \text{ mm}$	$l_{12} = 187 \text{ mm}$
$l_{13} = 430 \text{ mm}$	$l_{14} = 430 \text{ mm}$	$\omega_1 = 2 \cdot \pi \text{ rad/s}$

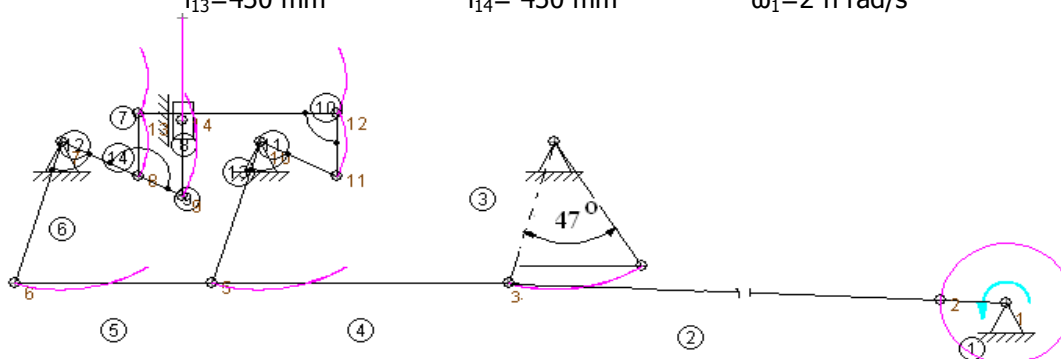


Fig. 3. Node path corresponding on complete rotation of motor element

Over the simulation is presented a few graphical dependences like, variation of relative angle (AR) with time, angular velocity (AV) with time, angular acceleration with time (AA). Angle input motion is considered a linear time dependence. In figure 4, 5, 6 is presented graphical dependences for bar element number 2, 3 and 10.

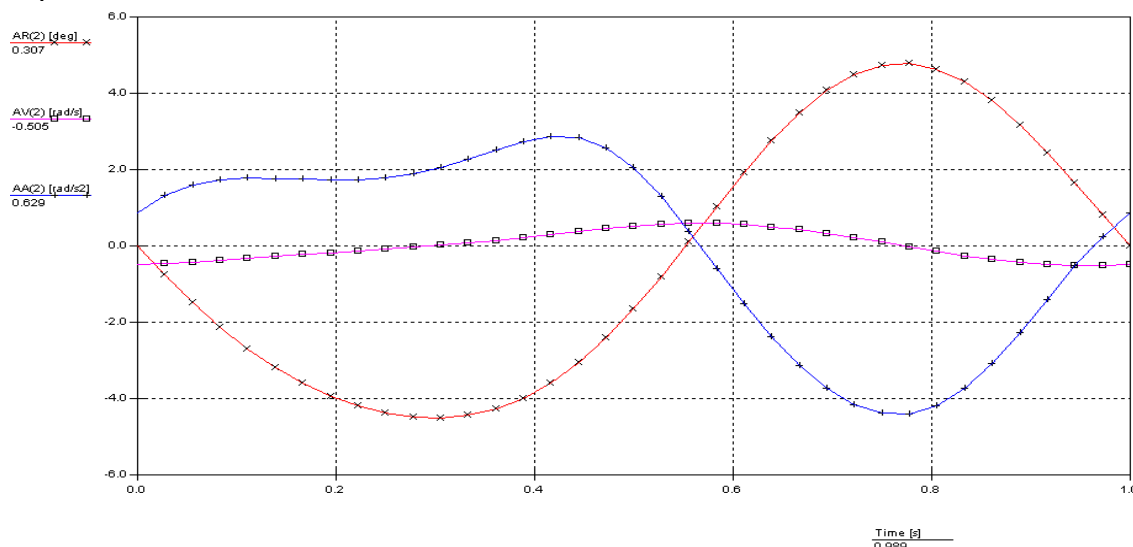


Fig. 4. Variation of relative angle , angular velocity and angular acceleration with time for bar element number 2

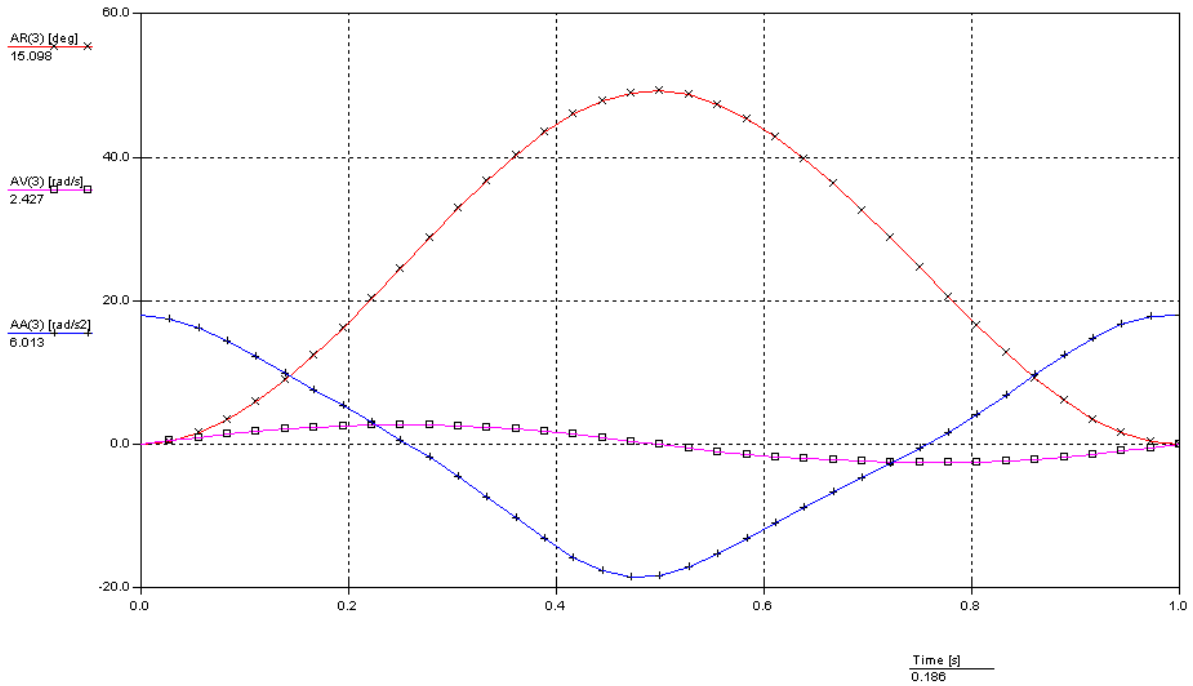


Fig. 5. Variation of relative angle, angular velocity and angular acceleration with time for bar element number 3

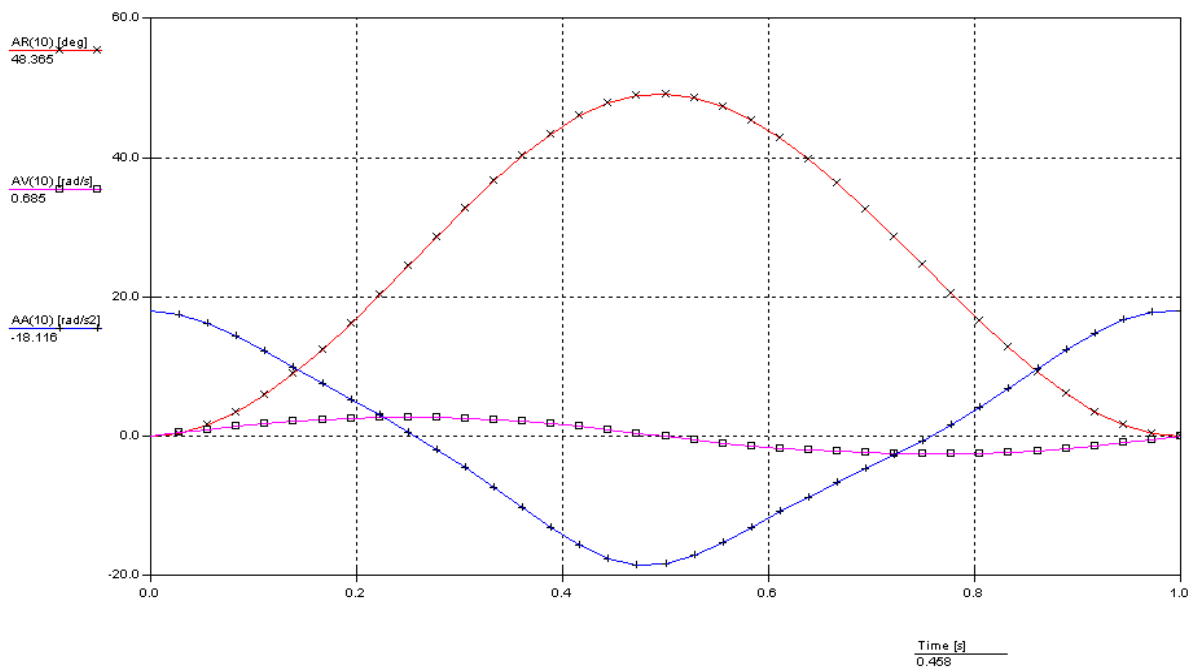


Fig. 6. Variation of relative angle , angular velocity and angular acceleration with time for bar element number 10

Also, is presented a graphical dependence like angle, angular velocity and angular acceleration with time for a few nodes in X-Y projection and absolute value in figure 7,8,9,10,11 and 12.

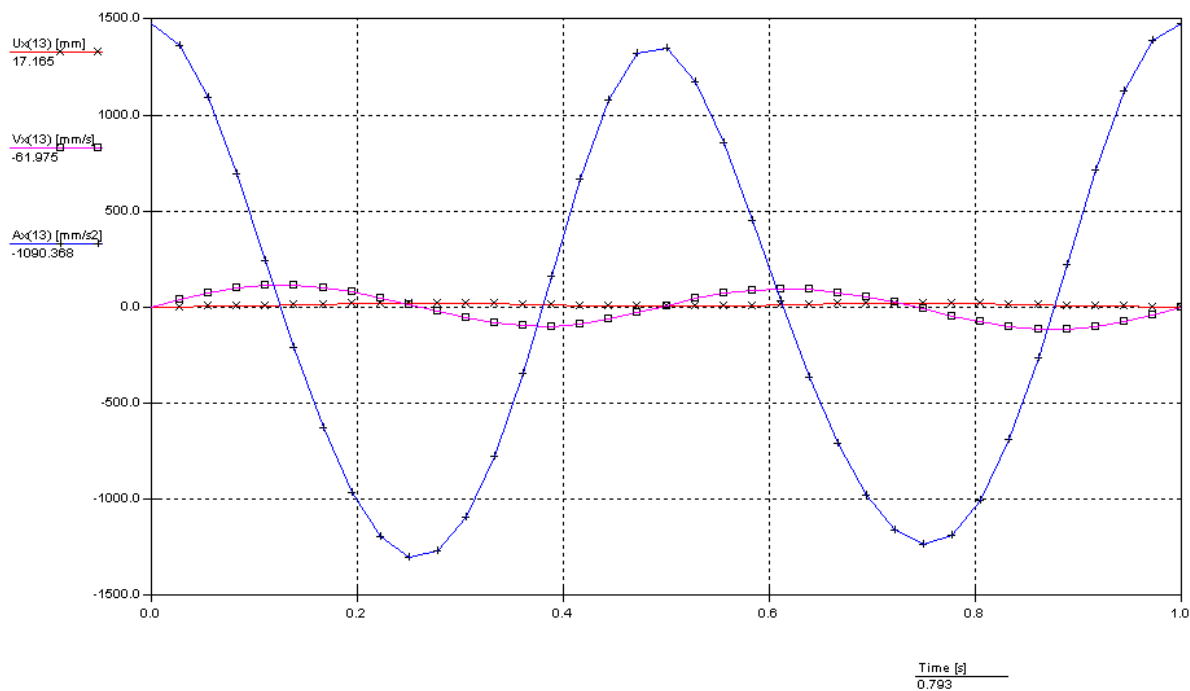


Fig. 7. Graphical dependence - angle, angular velocity and angular acceleration with time for nodes number 13, in OX projection

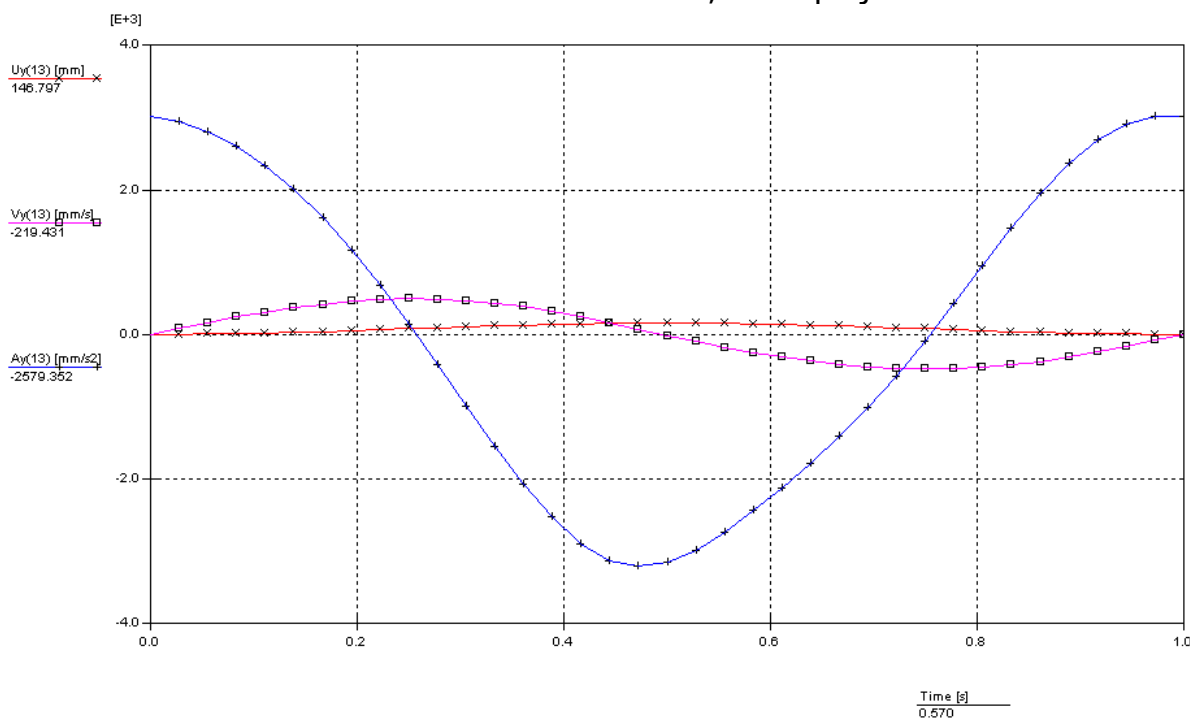


Fig. 8. Graphical dependence - angle, angular velocity and angular acceleration with time for nodes number 13, in OY projection

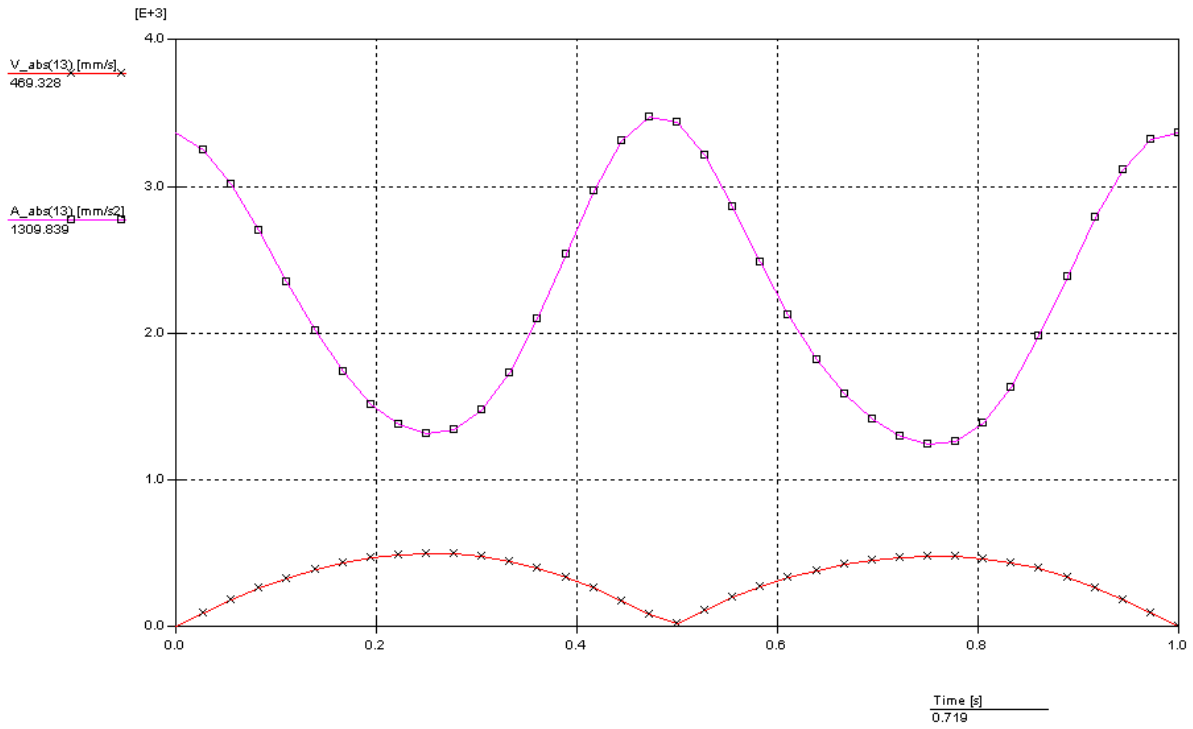


Fig. 8. Graphical dependence - angle, angular velocity and angular acceleration with time for nodes number 13, absolute values

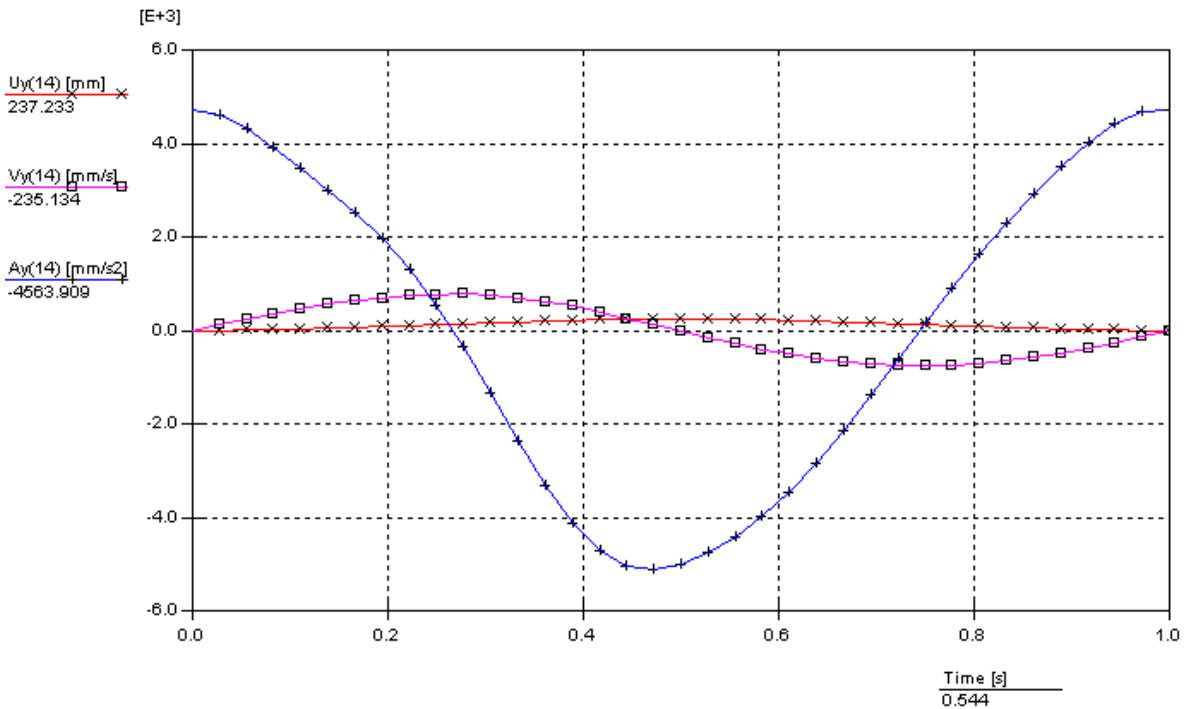


Fig. 9. Graphical dependence - angle, angular velocity and angular acceleration with time for nodes number 14, in OY projection

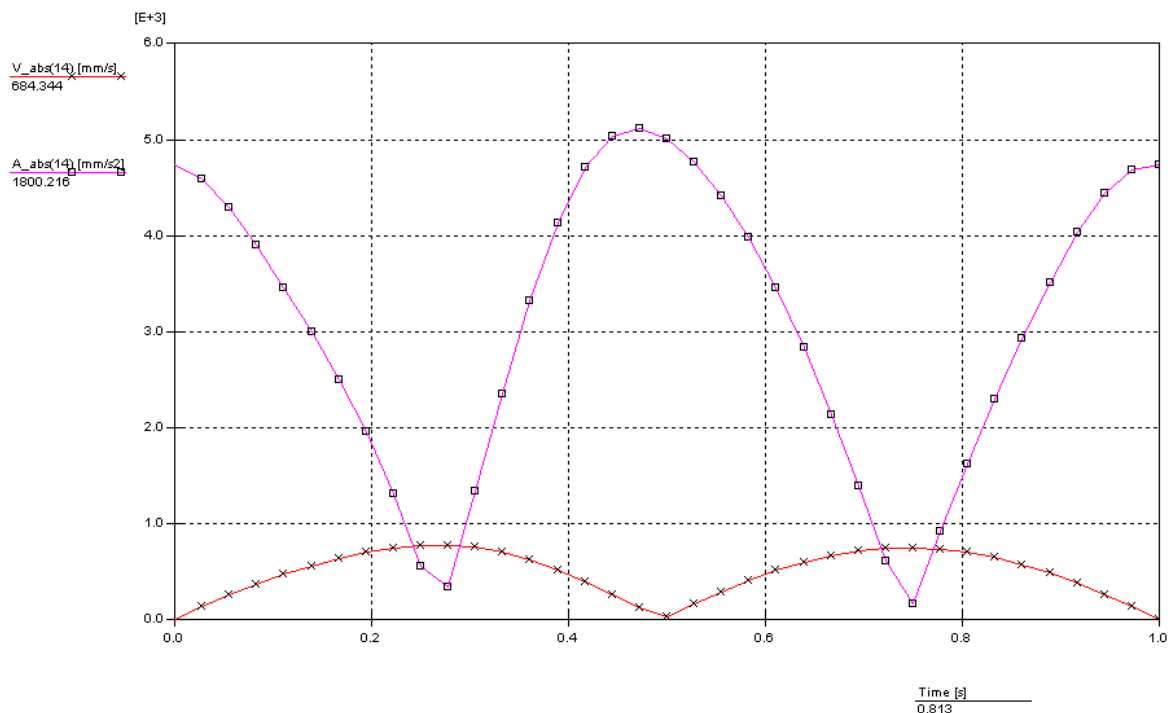


Fig. 8. Graphical dependence - angle, angular velocity and angular acceleration with time for nodes number 14, absolute values

3. CONCLUSIONS

Cinematic analysis is providing a lot of results, which are necessarily in cinetostatic analysis and in study of parts of first line braking mechanism. This analysis program permit a complex analysis of mechanism, and mechanism design is made in cad programs like AutoCAD.

4. REFERENCES/BIBLIOGRAPHY

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