

EXPERIMENTAL TESTING METHODS OF HARDOX 500 FACE MILLING BY PRAMET 8230 CARBIDE INSERTS

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ABSTRACT:

This article deal with the face milling proces of HARDOX 500. Material abrasion resistance HARDOX 500 have to discharge very hard inquires against mechanical wearing. Manufacturing process of this material is result of various factors effect as are combination of high strength, stiffness and toughness. The application in technical praxis is a result in general spectrum of usage e.g. working part of automatic feeder, jaws, crushers, stone crushers etc. The manufacturing process of HARDOX 500 sheets consists of hot sheeting between 900÷920 degrees in stabile austenite area and then directly hardened very fast in water shower. After low temperature annealing at 200÷300 degrees, then reaches the range 46÷50 Rockwell hardness. HARDOX is manufactured by SSAB Öxellösund (Sweden) and importer for Slovakia is WINFA Ltd. Trnava.

KEYWORDS: Hard face milling, PRAMET SNHF 8230 cutting inserts, cutting parameters, HARDOX 500, diagram of cutting tool wearing, milling cutter wear.

1. INTRODUCTION

HARDOX 500 – the abrasion resistance sheet verified the fundamental requirements for its hardness. It is important facility against mechanical wear. Very important basic factors from its production process result from high hardness, stiffness and toughness combination. Thermo-mechanical heat treatment causes improvement and increase as physical-mechanic properties. All these positive facilities predestinated HARDOX 500 for large spectrum of application. Experimental testing methods of HARDOX 500 face milling (Fig.1a, b) were realized by PRAMET milling cutter with 8230 changeable inserts SNHF 1204EN-SR-M1 (Fig.2a, b).

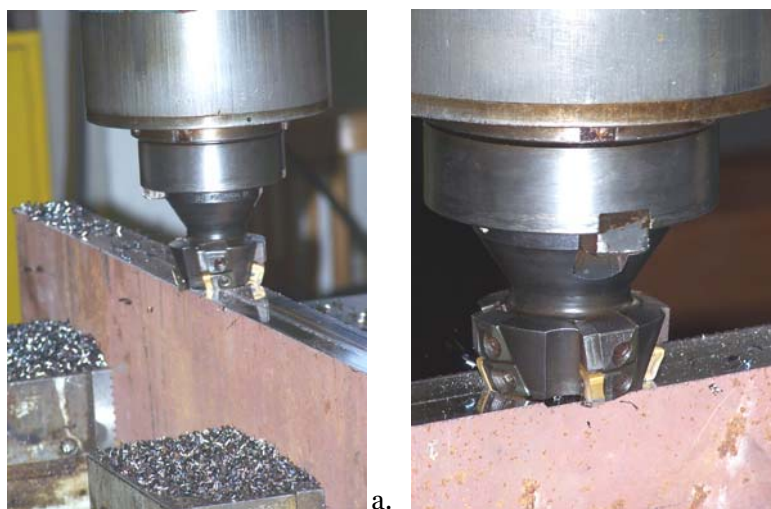


Fig. 1.a, b: Overall view for HARDOX 500 sheets clamping and face milling process at FA3V machine tool by PRAMET 8230 changeable inserts

2. WORKPIECE MATERIAL FOR EXPERIMENTAL FACE MILLING

Material: HARDOX 500 abrasion resistance sheet

Dimensions: 20x150x705mm created by laser (TRUMATIC L3030 – STELLIT Ltd.Trencin)

Hardness: 46÷50 HRC

Chemical composition: 0.29%C; 0.70%Si; 1.6%Mn; 1.0%Cr; 0.5%Ni; 0.3%Mo; 0.004%B; 0.025%P; 0.010%S

Manufacturing process: hot sheeting at 900÷920 degrees, then heat treatment in stabile austenite area, rapid hardening up to 1 min at water jet, low temperature annealing

3. EXPERIMENTAL MILLING PROCESS AND CUTTING CONDITIONS

Machine tool: FA3V vertical console milling machine, P = 45 kW

Cutting tool: NAREX milling cutter with changeable inserts, D = 50 mm, PN 222460.12, z = 4, K_r = 75 deg, rake angle γ = -7 deg, cutting clearance angle α = 7 deg, λ_s angle = -4 deg

Changeable cutting insert: SNHF 1204ENSR-M1-8230 PRAMET TOOLS (see on Fig.2a, b)

Workpiece material clamping: two pieces of sheet clamped in double grippers on machine tool support for 150 mm highness

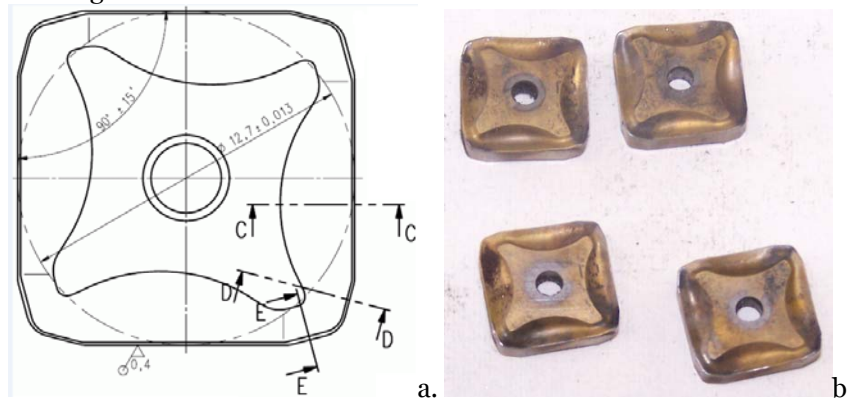


Fig.2 a, b: Applied cutting changeable inserts PRAMET, a) schematic image, b) real photo

Milling parameters: for $T = f(v_c)$ – where T is a function of cutting speed to Taylors ratio

Constant parameters:

Depth of cut $a_p = 2,0$ mm

Width of cut $a_e = B = 40$ mm

Allowed wear estimation $VB_k = 0,2$ mm

Revolution feed $f_0 = 0,224$ mm

Feed motion pre tooth $f_z = 0,056$ mm

Without coolant

Changeable parameters:

Cutting speed $v_{c1} = 55,7$ m/min

Spindle speed $n_1 = 355$ /min

Translation speed $v_{f1} = 80$ mm/min

Cutting speed $v_{c2} = 78,5$ m/min

Spindle speed $n_2 = 500$ /min

Translation speed $v_{f2} = 112$ mm/min

Cutting speed $v_{c3} = 111$ m/min

Spindle speed $n_3 = 710$ /min

Translation speed $v_{f3} = 160$ mm/min

Time of milling process and reached cutting durability:

$t_{AS1} = 8,86$ min, $t_{AS2} = 6,29$ min, $t_{AS3} = 4,40$ min

$T_1 = 223$ min, $T_2 = 135$ min, $T_3 = 39,6$ min

Milling time estimation: directly from formula $t_{AS} = L / n \cdot f_z \cdot z$

The graphs of wearing depending up of time you can see on (Fig.3a,b,c), where

a) $v_{c1} = 55,7$ m/min, b) $v_{c2} = 78,5$ m/min, c) 111 m/min.

Sequential relation $T = f(v_c)$ acquired from graphs and processed by square method is displayed on Fig.5 in double logarithmic axis system. This acquired relation from cutting durability to cutting speed has the final form:

$$T = \frac{2,4 \cdot 10^4}{v_c^{2,1}}$$

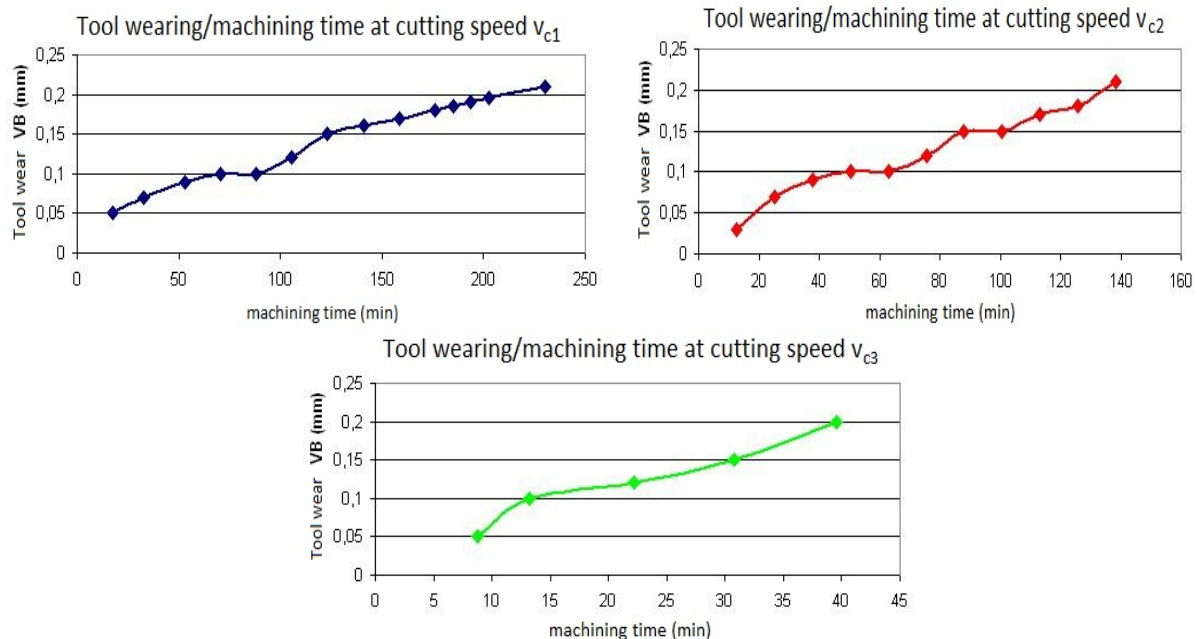


Fig.3 a, b, c: Generated graphs at various cutting speed during face millig process

4. THE FACE MILLING BY PRAMET 8240 WITH $T = f(f_z)$ VERIFICATION

The face milling process with the same tool holder NAREX PN222460.12 with 4 inserts was realized by the PRAMET changeable inserts 8240 SNHF1204ENSR-M1. Cutting conditions during milling were the same as in the previous process. The overall results from measured cutting times, inserts durability but at various feed motions $f_{z1} = 0.039$ mm/tooth; $f_{z2} = 0.056$ mm/tooth; $f_{z3} = 0.078$ mm/tooth; $f_{z4} = 0.112$ mm/tooth; $f_{z5} = 0.15$ mm/tooth were graphically executed. Then from these measured values at constant revolutions $n = 355$ /min were designated $T = f(f_z)$ by the square method to the final form: $T = C_T / f_z^y$. $T = 7.551 / f_z^{0,99}$. Reached surface roughness was reached by the feed motion growth in the range from $R_a = 0.6 \div 0.95$ μ m to $R_a = 1.2 \div 1.6$ μ m. The auxiliary cutting edge was also wear to $VB = 0.1 \div 0.12$ mm. See on Fig.4.

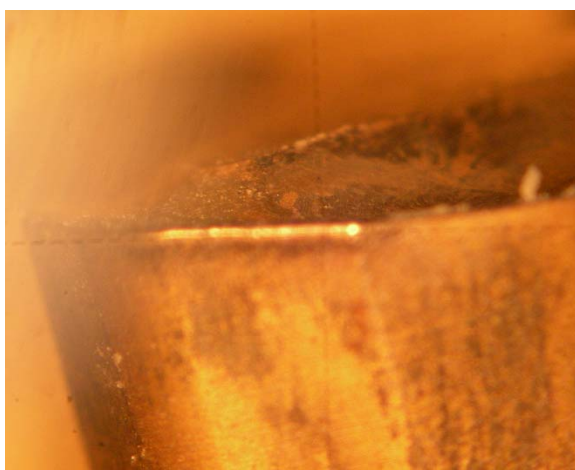


Fig.4: Tool insert wearing on auxilliary cuting side.
Measured on MITUTOYO TM 500 microscope
(extension 30x)

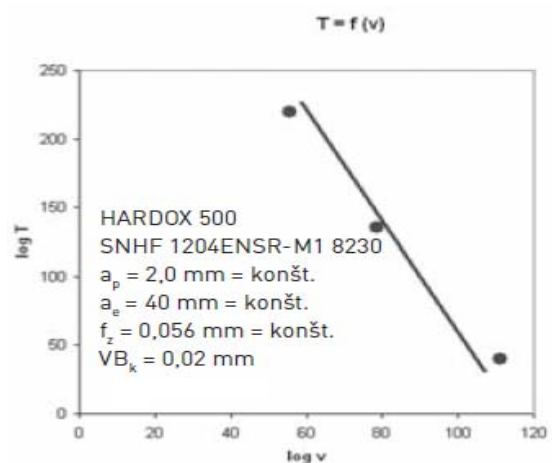


Fig.5: Sequential relation $T = f(v_c)$ in double logarithmic axis system

5. CONCLUSION

These experimental hard face milling process with PRAMET 8230 and 8240 show us that carbide insert 8230 has cutting durability $T = 223$ min whereas 8240 only $T = 132$ min, what is 68% more than with 8240. Both two types of coated cemented carbide inserts are desirable for hard machining technology application of HARDOX 500 with 46÷50 Rockwell hardness. 8240 is also desirable, but by lower cutting conditions. Face milling process is convenient without coolant in 8230 and 8240.

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